DOCUMENT-IDENTIFIER: US 4659511 A

TITLE: Method for solidifying radioactive waste

DEPR:

As still another embodiment of this invention, there will be described below,

with reference to FIG. 12, a case where not the pelletized radioactive waste

but the radioactive waste (mainly composed of Na.sub.2 SO.sub.4) generated from

a <u>nuclear</u> power station is directly treated and solidified in a 200-1 drum. In

this case, in order to secure the strength of the solidified waste and the

proper volume reduction ratio of the waste, the radioactive liquid waste

contained in a tank 12 is first dehydrated and formed into a
powder in a dryer

13 and then supplied into a tank 14. Various methods are known for drying the

radioactive liquid waste, such as centrifugal film drying, spray drying,

fluidized bed drying, drum drying, <u>freeze</u> drying and crystallization, and any of these methods can be employed in this invention.

CCOR:

588/4

CCXR: **588/14**

DOCUMENT-IDENTIFIER: US 4980093 A

TITLE: Method of treating high-level radioactive waste liquid

DEPR:

As described above, in accordance with the present invention, the high-level

radioactive waste liquid can be separated into (a) condensate (nitric acid

solution), (b) bulk wastes mainly containing sodium nitrate, sodium hydroxide,

etc., and (c) residue (nitrate) mainly containing <u>fission</u> products, actinoids,

and corrosion products (iron, chromium, nickel, etc.) in the reprocessing

process. As a result, (1) since the high-level radioactive waste liquid is

separated by the <u>freeze-vacuum-drying</u> process, (2) the problem of corrosion due

to high temperature is overcome, (3) and the condensate (nitric acid solution)

and bulk wastes mainly containing sodium nitrate and sodium hydroxide can be

converted into low-level radioactive waste. In addition, (4) if the residue

containing <u>fission</u> products, actinoids, and corrosion products (iron, chromium,

nickel, etc.) that have stable configurations as nitrate and roasted product is

stored in the form of residue, it is advantageous at the time when useful

elements (rhodium, palladium, etc.) <u>contained</u> in the residue (nitrate or

roasted material) are recovered in the future. Furthermore, (5) when a

glassified body is made, since the amount of sodium is small, a high-quality

glassified body can be formed, so that the amount of a glassified body produced

can be reduced substantially. Moreover, fractionated substances can be used as

raw material for artificial minerals (e.g., titanium, zirconium, calcium,

barium, aluminum) .

CCOR:

DOCUMENT-IDENTIFIER: US 3849330 A
TITLE: CONTINUOUS PROCESS FOR IMMOBILIZING RADIONUCLIDES,
INCLUDING CESIUM AND
RUTHENIUM FISSION PRODUCTS

DEPR:

Ĭ,

Advantageously, ruthenium <u>fission</u> products which are highly volatile and are

not immobilized in the complex metalo-silicate as are the other radio nuclides,

excepting of course cesium, will be reduced to ruthenium metal by either

elemental silicon or elemental aluminum and be separated with the other metals,

e.g., iron, rhodium, palladium, nickel, chromium, silicon via container 19.

When <u>container</u> 19 is filled, the temperature of the silicate melt is lowered by

cooling coils 20, <u>freezing</u> the silicate and <u>container</u> 19 consisting of a metal

ingot 21 containing noble metals (Ru, Rd, Pd) is disconnected from reactor 1

and an empty container is attached in its place.

CCOR:

DOCUMENT-IDENTIFIER: US 4115312 A

TITLE: Nuclear waste storage container with metal matrix

TTL:

Nuclear waste storage container with metal matrix

BSPR:

<u>Nuclear</u> waste storage containers containing a <u>metal matrix for</u> the nuclear

waste are desired to provide greater impact strength for the waste container

and to increase the thermalconductivity to prevent undesirably high centerline

temperatures. Matrix fabrication has been effected by casting, although this

process may prohibit the use of materials having high melting points which may

be required to prevent melting of the matrix during storage from unforeseen

temperature excursions or other accidents. Matrix fabrication by prior

processes has generally been concerned with low temperature metals such as lead and aluminum.

BSPR:

It is a further object of this invention to provide a storage container

containing high-level <u>nuclear</u> waste in a sintered <u>metal matrix</u>, which metal

matrix provides impact strength to the waste container and increases heat

transfer from the container interior to the container exterior to prevent

undesirably high centerline temperatures within the container.

DEPR:

The high-level waste particles that may be used in this invention may be

obtained from glass particle fabrication processes or ceramic particle

fabrication processes wherein the waste form utilizes existing calcining

processes with a compositionally modified waste liquid to achieve an improved

or supercalcine waste form in which generally all of the radioactive atoms will

be isolated in thermally and chemically stable phases. For

example, the high

level waste particles may be chemical vapor deposition alumina and pyrolytic

carbon coated improved ceramic particles or supercalcine ceramic particles, and

generally contain <u>fission</u> products as ceramic oxides or as glass modifiers.

The metal matrix powders that may be used are such as pure copper
and its

alloys, pure iron and its alloys, AISI Series 410, 304, 310 and 316 stainless

steels, and superalloys, such as Inconel or Hastalloy. A particularly good

copper alloy matrix is manganese bronze having a nominal composition, expressed

in weight percent, of 57.5 copper, 39.25 zinc, 1.25 iron, 1.25 aluminum, and

0.25 manganese. The properties of the matrix materials that are desirable are

a high melting point, good thermoconductivity, good mechanical strength, good

corrosion characteristics in salt, water, and/or air, and good oxidation

resistance in air at operating temperatures.

CCOR:

DOCUMENT-IDENTIFIER: US 5980602 A

TITLE: Metal matrix composite

BSPR:

It is still an additional object of the present invention to provide a method

for manufacturing an improved $\underline{\text{metal matrix}}$ composite material to result in a

material having superior hardness, strength, and density characteristics while

being extrudable and weldable for use in the manufacture of a variety of

structural members which may be readily connected to one another such as in

bicycle and other vehicle frames and components, engine components, aircraft

parts, tooling, sporting equipment such as tennis rackets, badminton rackets,

baseball bats, arrows, golf club shafts, and hockey and lacrosse sticks,

eyewear, automotive parts, electronic parts, furniture, medical equipment,

battery housings, nuclear shielding, marine components, robots, carts and

seats, gourmet cookwarė, toy casings, high-pressure containers, tank linings,

and armor, for example.

DEPR:

3. A $\underline{\text{metal matrix}}$ composite of aluminum alloy 6061 base metal material and 30

weight % boron carbide. This composite material is extrudable and exhibits a

tensile strength of $62.3\ \text{kpsi}$ and a yield strength of $58.4\ \text{kpsi}$. The

formulation may be used for structural stiffness for marine applications or

nuclear shielding since it has strength and corrosion resistance.

CCOR:

75/236

CCXR:

DOCUMENT-IDENTIFIER: US 5700962 A

TITLE: Metal matrix compositions for neutron shielding

applications

BSPR:

According to an aspect of the present invention, a neutron shield is made of a

boron carbide-metal matrix composite wherein the metal matrix material is

aluminum, magnesium, titanium, or gadolinium, or an alloy thereof. The

composite is formed by blending dry powders of boron carbide and the ${\tt metal}$

matrix material to uniformly mix the powders, and then subjecting
the powders

to high pressures to transform the powders into a solid body that is then

sintered to form a composite that can be extruded, cast, forged, welded, and

manufactured into structures for neutron shielding. Such structures include

containers for holding <u>nuclear</u> waste, and load-bearing plates for use in

neutron shielding structures in $\underline{\text{nuclear}}$ submarines and power plants.

CCOR:

DOCUMENT-IDENTIFIER: US 4814046 A

TITLE: Process to separate transuranic elements from nuclear

waste

BSPR:

The current proposed process for treating the waste IFR salt does not recover

the contained actinides, but converts the wastes into more readily disposable

forms. The waste salt is contacted with a cadmium-lithium alloy, a strong

reductant, to transfer nearly all of the actinides from the salt into the metal

phase. This also results in most of the rare earth <u>fission</u> products being

transferred into the metal phase. The treated salt is dispersed in a cement

matrix that is cast into corrosion-resistant metal containers. This waste is

highly radioactive because it contains **fission** product cesium and strontium,

but it may not require disposal in a deep geologic repository because it does

not contain significant amounts of transuranic elements. The cadmium-lithium

alloy that contains the actinides and rare earths extracted from the salt is

combined with other metal wastes. The mixture is retorted to vaporize the

cadmium and leave a metallic residue consisting of **fission** products, small

amounts of actinides, zirconium from the fuel alloy and fuel cladding hulls.

This residue is combined with a metal powder, such as copper, and pressed into

a solid ingot. The $\underline{\text{metal matrix}}$ is encapsulated in a corrosion resistant

container and, because it contains small, but significant amounts of TRU

elements, it must be buried in a geologic repository.

CCXR:

DOCUMENT-IDENTIFIER: US 4488990 A

TITLE: Synthetic monazite coated nuclear waste containing glass

BSPR:

Due to corrosion problems with the glass produced by this process, an

alternative process known as the cermet process, has also been developed. In

the cermet process an iron nickel base metal matrix contains the fission

product oxides from the high level waste. The cermet produced by this process

is a continuous electrically conductive $\underline{\text{metal matrix}}$ containing small particles

(about 1 micron) of waste oxide. The process is described more fully in U.S.

Pat. No. 4,072,501. The final sintered waste cermet articles produced by this

process could be in the form of pellets or rods. Currently cylindrical pellets

0.6 inches in diameter and 0.6 inches long are conveniently extruded.

CCOR:

588/11

CCXR:

DOCUMENT-IDENTIFIER: US 4383944 A

TITLE: Method for producing molded bodies containing highly

active radioactive

wastes from glass granules embedded in a metallic matrix

BSPR:

By proper selection of the glass-to-metal ratio, the size of the individual

granules or of the powder particles and the mixing conditions, a product is

obtained in which the glass granules or the glass powder containing the

radioactive waste <u>fission</u> products are discontinuously embedded in a continuous

metal matrix phase. The average interparticle space (.lambda.)
for the glass

granules is given by ##EQU1## where L.sub.3 is the average size (intercept

length) of glass granules and V.sub.M is the volume content of the metal phase.

The equation provides the interrelationship between .lambda., L.sub.3 and

V.sub.M to keep a proper distance (.lambda..gtoreq.L.sub.3) between the

discontinuously embedded glass granules. The time of mixing depends on the

sort of powders. Generally good distributions of the glass granules in the

metal matrices
particles--are which is to say discontinuity of the glass

obtained the more the condition is approached that ##EQU2## where .rho. means

density. If there should exist access to a granule or a powder particle from

outside the molded body by corrosion or leaching media, only this one granule

or particle is in contact with the environment, while all others remain

insulated. Substantial corrosion and leaching is thereby prevented.

CCOR:

588/11

CCXR:

DOCUMENT-IDENTIFIER: US 4383855 A

TITLE: Cermets and method for making same

DEPR:

As briefly pointed out above, the cermets of the present invention may

incorporate radioactive waste in quantitites up to from 1 to about 75 wt.%

without deleteriously affecting the cermet quality. In making radioactive

waste cermets, compositional adjustments to the urea heavy-metal bearing

admixture may be necessary to ensure the formation of a desired metal matrix

and ceramic phases to provide the cermet with high density, thermal

conductivity, mechanical integrity, self-shielding properties, and resistance

to corrosion or leaching. Further, compositional adjustments may include the

addition of iron, nickel, copper, molybdenum, tin, lead, and the like for

providing sufficient oxide for the liquid-phase sintering operation to assure

that the particulate material, including nonreduced oxides, metals, and other

impurities that are present in radioactive waste, is microencapsulated within

the cermet. It may be also desirable to adjust the ceramic portion of the

cermet to include additives such as the oxides of zirconium, titanium,

aluminum, silicon, phosphorus, manganese, barium, and calcium. These oxides

are precursors to the formation at elevated temperatures of known fission

product immobilizing and retentive phases, such as: hollandite, perovskite,

zirconolite, nepheline, monazite, fluorite, spinel, leucite, pollucite,

scheelite, opatite, and kalsilite. See, for example, Ringwood, A. E., et al,

"The SYNROC Process: A Geochemical Approach To <u>Nuclear</u> Waste Immobilization,"

Geochem. J., 13, pp. 141-165 (1979); and Boatner, L. A., et al, "Monazite and

Other Lanthanide Orthoposphates as Alternate Actinide Waste Forms," The

Scientific Basis for <u>Nuclear</u> Waste Management, Vol. II, C. J. Northrup, Ed., Plenum Press, New York, New York (1980).

DEPR:

In order to further illustrate and demonstrate the effectiveness of the present

invention, a typical manufacturing operation is set forth below. A simulated

thorex waste solution, such as obtained from <u>Nuclear</u> Fuel Services-type thorex

waste, was prepared by admixing iron, nickel, copper, cobalt, and thorium in a

dilute nitric acid. This admixture was concentrated by sufficient heating to

drive off water. This solution was then contacted with molten urea and

precipitated at above 180.degree. C. The recovered precipitate was then

calcined at 800.degree. C. to provide an admixture of various calcined

powders. These powders were mixed with a water binder and cold pressed into a

green pellet of a size in a range of about 10.times.10 mm. This pellet was

placed in a furnace under hydrogen atmosphere and heated from room temperature

to a temperature of about 1500.degree. K. over a fifteen minute period.

During this heating, the selected oxide mixture in the pellet was sufficiently

reduced to a substoichiometric or suboxide value to provide the liquid phase

necessary for sintering the remaining particulate material when the temperature

increased to a level greater than the eutectic temperature of approximately

1300.degree. K. The sintered pellet was removed from the furnace and cooled to

room temperature in a reducing atmosphere. The resulting article was examined

and found to be structurally sound and shock resistant.

Metallographic

examination revealed that all oxide particles were tightly encapsulated within

a uniformly dispersed continuous metal matrix.

CCXR: **75/951**

DOCUMENT-IDENTIFIER: US 4338215 A

TITLE: Conversion of radioactive wastes to stable form for

disposal

ABPL:

Radioactive waste material, such as that resulting from radioactive weapons

plant operation or from nuclear fuel reprocessing, in suitable form, such as

radionuclide-containing oxide and/or oxyhydroxide and/or hydroxide particles,

is held by a metal or metal "alloy" to an electrically conductive cathodic

material upon which the metal or alloy is electrodeposited. In this way the

radionuclide species including strontium and/or cesium, which are biologically

extremely hazardous, are incorporated into a metal matrix held to a base and

may be disposed of, as by underground storage, in such form, which is

considered to be more resistant to dissolution by ground water and to damage by

mechanical stresses arising from tectonic activity than are glasses or ceramics

incorporating radionuclides. In improvements of the process and of the

resulting radionuclide-including article, the article is electrolytically or

otherwise covered or coated with suitably corrosion resistant and mechanical

damage resistant covering(s) or coating(s), as by continuing electrodeposition

of the metal, sometimes after addition of more material, which is a source of

the metal, to a suitable electrolyte, or after replacement of the electrolyte.

BSPR:

In accordance with the present invention there is provided a method for

converting radioactive waste material into a stable article for disposal or

storage which comprises electrolyzing a bath containing ions of a corrosion-resistant, electrodepositable metal or of a plurality of materials

including at least one such metal, in the presence of a solid state radioactive

waste material which contains a radionuclide selected from the group consisting

of strontium 90 and cesium 137 and mixtures thereof in one or more oxide and/or

oxyhydroxide and/or hydroxide forms so that the metal or materials including

metal is/are deposited on a cathode and bind(s) the radioactive waste thereto.

Preferably, the radioactive waste treated is calcined weapons waste or wastes

from $\underline{\text{nuclear}}$ fuel reprocessing, the cathode and the $\underline{\text{matrix metal}}$ are of copper

or other similarly corrosion resistant and electrodepositable metal, and the

electrolyte dissolves little, if any, of the radionuclide compound(s) of the

waste, e.g., 5% or less, preferably less than 0.5 or 0.1%. Also, it is

preferred that the article resulting from the process described be covered or

overcoated, either electrolytically or otherwise, with a corrosion resistant •

metal or other suitable coating, as by continuing electrodeposition of the

matrix metal after consumption of all or substantially all of the
radioactive

waste material, or by electrodeposition of covering metal or alloy from a new

or replenished bath. While the plating metal may be codeposited with finely

divided particles of radionuclide compounds, it is sometimes preferable to

pelletize the radionuclide compounds resulting from treatment of the waste and

then hold them to a conductive substrate by simultaneously metal coating them

and the substrate. In such operations, and when fine particles of radionuclide

compound are being electrodeposited, it may be desirable to treat the pellets

or powders first, as by coating or mixing with conductive powder, to increase

surface electrical conductivity and to reduce solubility. The described

process may be continuous or of the batch type. Also within the invention are

the described articles and a method for disposal of radioactive waste materials

in the form of such an article .

DEPR:

In FIG. 5 the step represented by numeral 39 is the conversion to a sludge or

slurry of an aqueous <u>nuclear</u> waste solution or suspension. This is usually

effected by evaporation of the continuous medium and the product resulting may

contain insoluble particles of radionuclide(s), preferably in oxide,

oxyhydroxide and/or hydroxide forms. However, such conversion to a sludge or

slurry may be by other means, including sorption by zeolites and the

utilization of thickening or solidifying agents or other materials, which may

promote subsequent drying of the waste solution or obtaining of desirable forms

thereof after drying. In some cases the $\underline{\text{nuclear}}$ waste suspension may be

evaporated directly, despite being relatively dilute, but usually for best

evaporation a thickened liquid or sludge will be preferred as a starting

material. Drying or calcining of the sludge, usually to oxide, oxyhydroxide or

hydroxide form, preferably to the oxide, is effected at step 41 and, although

it is not shown, the dried product may be further size reduced, agglomerated or

pelletized for best dispersion and/or most desirable settling and codeposition

rates and characteristics, e.g., reduced solubility in the electrolyte.

Increasing particle size helps to diminish solubility and so is often

preferable. Before or after such size changing operation (or in the absence of

it) it is preferred that to promote codeposition the conductivity of the

normally poorly conductive or even insulating oxides will be increased, as by

electroless deposition thereon of conductive material, intimate mixing with a

finely divided conductor, spray treatment with metal or other application of a

conductive substance or substances to the dried particles.

Often, metals are

preferred as the conductive materials, but graphite, especially colloidal

graphite, has also been found to be very useful. After

```
subjection of the
particles to a suitable conductivity increasing operation 43
(which may
sometimes be omitted), the produce thereof (if finely divided) is
dispersed in
a metal salt solution (usually an aqueous electrolyte) for
codeposition of the
radionuclide-containing compound and metal onto a metal base.
The making of
the metal salt solution is represented at 45 and the solution is
shown mixed
with and utilized with the radionuclide-containing compound in
electrodeposition step 47. In FIG. 4 coating onto one major
surface of a
conductive cathode is shown and in codeposition step 47 such
coating is
effected and additionally, coating of the other major surface of
the cathode
may be carried out after a 180.degree. rotation thereof
subsequent to
depositing of a sufficient thickness of metal
matrix-radionuclide-containing
compound on the first major cathode surface. Step 49 of FIG. 5
represents a
subsequent electrolytic coating of the article with a suitable
protective metal
or binary metal alloy (which may or may not be the same as the
matrix material)
to provide additional corrosion resistance. While such step is
highly
preferred, it is within the present invention to utilize the
uncoated article
of operation 47, and it is also within the invention to utilize
such product
when it is coated on only a single surface (usually a major
surface) of the
cathodic base material. After completion of the coating
operation, represented
in step 49 (after 47 if subsequent coating is not used) the
article is stored
or disposed of, as at 51, preferably being ultimately disposed of
in safe
underground storage. The process described is also readily
adaptable to
electrolytic (and electroless) deposition of pellets or
comparatively large
bodies of rad-waste onto base materials.
```

CCOR:

DOCUMENT-IDENTIFIER: US 4209421 A

TITLE: Method of preparing bodies containing radioactive

substances

BSPR:

For the safe final disposal of highly radioactive wastes, it is known to add

glass formers to them and, by known methods, to melt a glass therefrom which,

after solidification, can be stored in the form of monolithic glass blocks in

an appropriate container. Furthermore, products of extra safety margin have

been developed, such as aggregates of glass and metal, in which the highly

radio-active glass in the form of particles, which may be of sizes between two

and eight millimeters, is embedded in a <u>metal matrix</u> (W. Heimerl, Atomwirtschaft-Atomtechnik, 20 (1975) pp. 347-349). In other methods, the

highly radioactive glass block of appropriate composition is subjected to a

controlled devitrification by a suitable heat treatment; examples of the kind

of glass ceramics which have been proposed for formation by this method are

those of the celsian, perowskite, diopside and eucryptite type (A.K. De, B.

Luckscheiter, W. Lutze, G. Malow, E. Schwiewer, S. Tymochowicz, Management of

Radioactive Wastes from the <u>Nuclear</u> Fuel Cycle, IAEA, Vienna 1976, Vol. II, pp. 63-73).

CCOR:

588/15

CCXR:

DOCUMENT-IDENTIFIER: US 4204975 A

TITLE: Method and apparatus for encapsulating radioactively

contaminated lumps

or granular material in metal

DEPR:

The apparatus for carrying out the method of the invention can be used to

advantage for encapsulating spent nuclear fuel particles of the kind used in

high-temperature $\underline{\textbf{nuclear}}$ reactors. These particles consist of a core of

uranium carbide that was encased in a three-fold coating of pyrolytic carbon,

silicon carbide and pyrolytic carbon. The diameter of the uranium carbide

cores thus coated was between about 400 and 500 .mu.m. The spent nuclear fuel

particles encased, according to the process of the invention, with aluminum as

the $\underline{\text{matrix metal}}$, were suitable for final storage after the riser pipe 9 and

the air-removal pipe 8 had been pinched off. Instead of pinching off the tube

ends, it is of course also possible to close them in some other way, for $\ensuremath{\mathsf{T}}$

example by welding.

CCOR:

DOCUMENT-IDENTIFIER: US 4072501 A

TITLE: Method of producing homogeneous mixed metal oxides and metal-metal oxide

mixtures

DEPR:

The simulated **fission** products and nickel were dissolved as nitrates in a

minimum amount of 1 M HNO.sub.3, about 180 ml. Sufficient solid urea was added

to provide about 20 grams of oxides per liter of urea. The solution was heated

to 130.degree.-140.degree. C for 1 hour to remove the water of dissolution and

hydration, after which the temperature was raised to about 180.degree. C for

40-50 minutes to precipitate the metal values. All the metal values

precipitated homogeneously. The molten urea mixture was heated to 400.degree.

C for sufficient time to evaporate the urea leaving a dry powder. This dried

powder was heated to 800.degree. C in air for calcining, forming a mixture of

nickel oxide and simulated **fission** and corrosion product oxides. The dried

powder was heated at 850.degree. Ć for 1 hour in hydrogen atmosphere,

whereupon the nickel oxide was reduced to metal powder. The metal values from

simulated <u>fission</u> products were still present as oxides having typical particle

size of 0.2 microns. The powders were homogeneously mixed. The mixture was

consolidated by hot pressing at 1100.degree. C and 4000 psi for 1 hour to form

a cermet waste immobilization article containing **fission** products within a

continuous nickel matrix. Scanning electron microscopy revealed that each

oxide particle was completely surrounded by the metal matrix.
For waste

immobilization articles, the $\underline{\mathtt{matrix}}$ metal can be 50 to 70 volume \$ of the

article. If desired, a ceramic waste immobilization article can be prepared by

eliminating the reduction step and hot pressing the oxide powder mixture.

Cermet waste immobilization articles are substantially more ductile and

thermally conductive than ceramic waste articles. The present process is

particularly advantageous for preparing radioactive powders and for other

applications requiring remote handling, since the solids are separated from

solution by evaporation rather than filtration. Filtration processes are

generally to be avoided in handling hazardous substances, e.g., nuclear fuel

reprocessing operations, in order to preclude the formation of aqueous effluents.

CCOR:

75/344

CCXR: **75/365**

DOCUMENT-IDENTIFIER: US 5879110 A

TITLE: Methods for encapsulating buried waste in situ with molten wax

BSPR:

In the early days of the nuclear age, contaminated debris and undocumented low

level radioactive waste were buried in shallow trenches. Other waste materials

were placed in underground storage tanks. These burial areas are now

considered to pose a unacceptable risk to the environment. Excavation and

removal of these wastes is potentially dangerous and very expensive. The

concern is that excavation of such sites could release airborne radioactive

contaminants which would pose a substantial harm to personnel and nearby

residents. There have been a number of solutions proposed for containing these

sites. Some of these solutions include slant drilled jet grouting, soil

freezing, soil dehydration, tunneling, and chemical grout
permeation. Others

have taught vertical drilling and hydraulic fracturing as a means of forming a bottom barrier.

CCXR:

DOCUMENT-IDENTIFIER: US 5905184 A

TITLE: In situ construction of containment vault under a

radioactive or

hazardous waste site

BSPR:

In the early days of the <u>nuclear</u> age, contaminated debris and undocumented low

level radioactive waste were buried in shallow trenches. Other waste materials

were placed in underground storage tanks. These burial areas are now

considered to pose a unacceptable risk to the environment. Excavation and

removal of these wastes is potentially dangerous and very expensive. The

concern is that excavation of such sites could release airborne radioactive

contaminants which would pose a substantial harm to personnel and nearby

residents. There have been a number of solutions proposed for containing these

sites. Some of these solutions include slant drilled jet grouting, soil

freezing, soil dehydration, tunneling, and chemical grout
permeation. Others

have taught vertical drilling and hydraulic fracturing as a means of forming a bottom barrier.

CCOR:

588/260

CCXR:

DOCUMENT-IDENTIFIER: US 5890840 A

TITLE: In situ construction of containment vault under a

radioactive or

hazardous waste site

BSPR:

In the early days of the <u>nuclear</u> age, contaminated debris and undocumented low

level radioactive waste were buried in shallow trenches. Other waste materials

were placed in underground **storage** tanks. These burial areas are

considered to pose a unacceptable risk to the environment. Excavation and

removal of these wastes is potentially dangerous and very expensive. The

concern is that excavation of such sites could release airborne radioactive

contaminants which would pose a substantial harm to personnel and nearby

residents. There have been a number of solutions proposed for containing these

sites. Some of these solutions include slant drilled jet grouting, soil

freezing, soil dehydration, tunneling, and chemical grout
permeation. Others

have taught vertical drilling and hydraulic fracturing as a means of forming a bottom barrier.

CCXR: